CHAPTER IV

CHIMNEY TABLES, WIND-PRESSURE, AIR-SPACE IN GRATES

RATE OF COMBUSTION

The results of 45 tests of boilers with anthracite and Welsh steam coal give only 5 instances where the rate of combustion was greater than 13 pounds of coal per square foot of grate per hour, and all of the tests showed the rate of evaporation from and at 212° Fahr. per pound of combustible to be 8.11 pounds to 14.23 pounds.

The same quantity of coal as used in the above tests, burned on a smaller grate, evaporated more water per pound.

Averages of 15 tests by Isherwood give the following data:

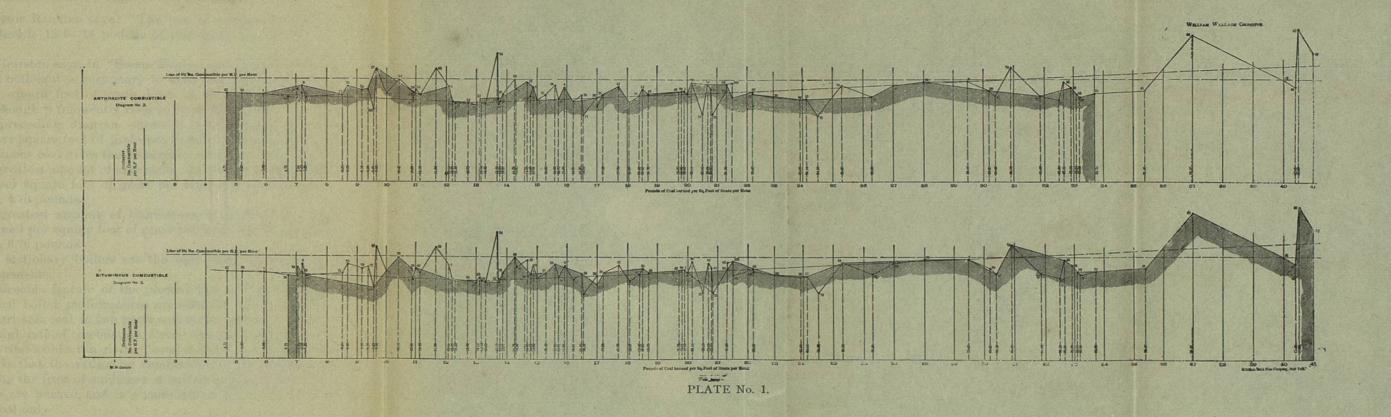
	Coal per sq. ft. of grate per hour.	Evaporation from and at 212° F. per lb. coal.
Anthracite coal	12.75	8.90
Semi-bituminous coal	10.95	10.14
Bituminous coal	12.43	9.31

Another case—Average of 15 boilers tested gives 13.87 pounds of coal to square foot of grate per hour, while only 7 tests exceed 13 pounds (capacity trials).

For economy trials we have the average of 15 tests, giving 9.77 pounds of coal per square foot of grate per hour; none being over 13 pounds.—Clark, Volume I.

Thurston—"Steam Engine and Boiler Trials," p. 17, says the "efficiency of fuel falls off at 50 to 60 pounds of fuel burned per square foot of grate" (per hour).

In the plotted tests of the writer, PLATE I, all regularity ceases after 37 pounds of coal burned per square foot of grate is reached.



The following averages are from over 100 tests collated by the writer:

Professor Rankine says: "The rate of combustion in factory boilers is 12 to 16 pounds of coal to the square foot of grate."

Dr. Thurston says, in "Steam Engine and Boiler Trials":
"In land boilers it is customary to keep the rate of combustion per square foot of grate down to about 8 pounds per hour, although it frequently rises to 10 or 12 pounds."

The preceding diagram shows that 13 pounds of coal burned per square foot of grate per hour of either anthracite or bituminous coal gives the greatest economy in evaporation.

The greatest amount of anthracite coal found to have been burned per square foot of grate per hour was 33.70 pounds; the least, 4.70 pounds.

The greatest amount of bituminous coal found to have been burned per square foot of grate per hour was 57 pounds; the least, 6.70 pounds.

Land stationary boilers are the only ones considered in these statements.

A noticeable feature of the plotted data is that the most economical boiler performances are obtained when a mixture of one part soft coal to two parts anthracite dust is burned at quite a high rate of combustion, forced draught being used.

The writer's object in giving "combustible" per square foot of grate is that the rating by combustible is the best way of comparing the tests of a number of boilers under which different coals are burned, and is a more reasonable criterion than that of coal only.

It will be readily seen from the averages that less than 4 pounds of coal in the majority of cases is that which is required to be burned per hour to produce one horse-power; and as 13 pounds of coal burned per square foot of grate is a most economical rate of combustion, 13 divided by 4, or 3.25 horse-power per square foot of grate per hour, is most economically attainable.

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The above is for anthracite coal. For bituminous coal, as 23.8 pounds burned per square foot of grate is an economical rate of combustion, 23.8 divided by 4, or 5.95 horse-power per square foot of grate per hour, is economically attainable.

The average of 13 and 23.8 is 18.4, which is very nearly 18.16, the average of all the 108 tests; which confirms the correctness of common practice, as to rates of combustion.

CHIMNEYS.

The writer has found that a relation exists between the coal burned per square foot of grate, with efficient chimney draft, for anthracite and bituminous coal, and by assuming that

coefficient $\times A \sqrt{H} = \text{coal}$ per hour in pounds, then coefficient $\times A \sqrt{H} = G \times \text{coal}$ per square foot of grate per hour, we find that for anthracite coal the coefficient equals the coal burned per square foot of grate, and that for bituminous coal the coefficient equals the coal burned per square foot of grate divided by 1.83.

The following tables, figured by formulæ given, will give satisfactory results to any who may use them; should any special modification be needed, the user must use his own judgment with regard to them.

Table No. 6. Grate area for a rate of combustion of 13 pounds per square foot of grate per hour.

Table No. 7. Grate area for a rate of combustion of 23.8 pounds per square foot of grate per hour.

Table No. 8. Coal capacity of chimney.

Table No. 9. Horse-power of boilers.

Table No. 10. Horse-power of chimneys, when two pounds of coal per hour burned furnishes one indicated horse-power at engine. Should the engine horse-power be known, and the chimney size wanted, great care should be exercised in determining it.

The last table is intended only for the one case. The writer has put himself on record as being decidedly in favor of rating chimneys at their coal capacity and not by horse-power. The 23.8 is a derived constant obtained by multiplying 13 × 1.83; 1.83 confirms Mr. Harris's rule for grate area for bituminous coal burned with natural draft, 23.8 is an economical rate of combustion for bituminous coal.

A horse-power is understood throughout these tables to be the American Society of Mechanical Engineers' standard of 34½ pounds of water evaporated per hour from and at 212' Fahr.

	AREA						HEIGHT	HEIGHT OF CHIMNEY	MNEY							FOILIN
	3	200	,09	70,	80,	,06	100,	110	126'	150	176	200,	225	250	300	8q. Chim.
Inches.	Sq. Ft.			10	ate Are	V=(0) ¤	VH for	a rate o	Grate Area (G): AVH for a rate of combustion of 13 lbs	stion of	13 lbs.					Side of 8q
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1	3.98	28	,37	33	35	38										2,2
0	4.91	35	88	41	44	47	40									
88	5.94		94	20	53	56	59	69		1	1	-		1	1	- 27.
8	7.07	The state of the s	99	69	63	67	70	74	7.0				400			30
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	000															9
1 0	+ 70.07		-	18	98	91	96	102	108	120					1000	00
2	14.07				112	119	126	132	141	157				-	-	40
+ <	10.90					151	159	187	178	199	210					2 9
0	19.64					186	198	206	220	246	260					2 4
9	98.78						000									
2	28.27			1		-	986	248	266	297	874	336	1.01		-	69
78	33.18						3	948	971	415	410	400	474	-		99
*	38.48						102	403	4.87	481	500	F44	490	070	000	2:
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+	44.18			-				-	495	689	584	808	000	000	100	00
	50.27				The same of		100		563	898	RRK	711	754	200	007	200
~	66.75	Sheet Line							636	709	740	608	201	000	1000	000
_	63.62								712	795	841	800	954	1008	1701	98
	70.89															:
-	78.54									-886	937	1002	1063	1727	1228	101
~	95.03			1	BOUT B	STATES!				882	1038	1111	1178	1242	1360	107
の地	173.10						-	The state of		1188	1256	1344	1425	1502	1646	117
	á						N. Contract of the Contract of			+1+1	1495	1830	1691	1788	1959	128
200									Date of			Contract of				
1											The Control		-	No.		
1	我們	+	1													

DIAM	AREA					H	EIGHT O	F CHIM	NEY.							EQUIV.
	(A)	50'	60'	70'	80	90'	100'	110'	125'	150'	175'	200'	225'	250'	300'	Sq. Chim
Inches.	Sq. Ft.		6	irate Ar	ea (Gy) =	AVH ÷	1.83 fo	r a rate	of com	bustion	of 23.8	lbs.				Side of 8
18	1.77_	7	7.6	8.1	8.7											16"
21 24	2.41 3.14	9	10	11 14	12 15	16										19 22
27	3.98	15	17	18	19	21										24,
30	4.91	_19	21	23	24	26	27_									27
33 36	5.94 7.07		25 30	27 32	29 34	30 36	32	34 40	43							30 32 35
39	8.30			38	40	43	45	47	51							35
42	9.62			44	47	50	53	56	59	66_						38 43
48 54	12.57 15.90			THE RE	60	65 83	69 87	72 91	77 97	86 109	115					48
60	19.64					102	107	113	120	134	142					54
66	23.76						_130	136	145	162	172	184_				59
72 78	28.27 33.18				1		155	162 190	173 203	193 227	204	219 256	232	297		64 70
84	38.48	1						220	236	263	278	297	315	332	364	75
90	_44.18_								_270	302	319	341	362	381	472	80
96 102	50.27 56.75								308 347	343 388	353 410	389 439	412 465	434 490	476 537	86 91
108	63.62								389	434	459	492	521	550	602	96
114	70.88_									484	512	548	581	612	671_	101
120	78.54				2700					536 650	567 686	607 735	647 778	679 831	743	107
132 144	95.03 113.10			585			LES !			772	817	874	927	977	1070	128
							TO S									
				10.00	100	1	Bell			1		1			THE .	
						70.0		Ellin				9				

TABLE No. 8.

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18 1. 21	77	62 78 101 124 149	49 65 85 107 133 163	52 68 91 114	98 124	5 AVH;4	lbs. of c	oal burne	ed consid	lered 1 H	I. P.				16"
21 2- 24 3. 27 3.1 30 -4. 33 5.1 36 7. 39 8. 42 9.1 48 12.	41 55 14 72 98 91 91 114 94 07 30	62 78 101 124 149	65 85 107 133 163	68 91 114 143	124										19
21 2- 24 3. 27 3.1 30 -4. 33 5.1 36 7. 39 8. 42 9.1 48 12.	41 55 14 72 98 91 91 114 94 07 30	62 78 101 124 149	65 85 107 133 163	68 91 114 143	124										
24 3. 27 3.1 30 4. 33 5.1 36 7. 39 8. 42 9.4 48 12.	14 72 98 91 91 114 94 07 30	78 101 124 149	85 107 133 163	91 114 143	124						Marie 1		SUSCENSION OF THE PERSON OF TH		
27 3.1 30 4. 33 5.1 36 7. 39 8. 42 9.1 48 12.	98 91 91 114 94 07 30	101 124 149	107 133 163	114	124								2 0 2 100		22
33 5.1 36 7.1 39 8.1 42 9.1 48 12.	94 07 30	149	163		153	STILL SOUTH			2.						24
33 5.1 36 7.1 39 8.1 42 9.1 48 12.	94 07 30	149	163			159									27
36 7.4 39 8.4 42 9.4 48 12.	07 30	179	192		182	192	202						The same		30
39 8 42 9.4 48 12.	30			205	218	228	241	257			10 60		100		32
48 12.			224	241	257	270	283	302							35
48 12.	62		263	282	296	312	332	351	390						38
	.57		THE REAL PROPERTY.	364	387	410	429	458	510					EKT	43
54 15.	90		1		491	517	543	579	647	683					48
60 19.	64				605	637	669	715	797	845					54
66 23.	76					774	809	865	965	1021	1092				59
72 28.	.27			TO THE	EN SEL	920	962	1051	1147	1215	1300	1378			64
78 33.	.18	1	4	SST.	1	1	1131	1206	1349	1459	1524	1619	1706		70 75
84 38.	.48						1310	1401	1563	1654	1768	1875	1976	2165	10
90_ 44.	19							1609	1794	1898	2031	2155	2269	2486	80
96 50.					Many and			1830	2041	2161	2311	2451	2584	2831	86
102 56.		100	379	35000	9-11-12	10 A 10 A	1	2067	2304	2434	2607	2766	2915	3195	91
108 63.			1	1	F.F.		100	2314	2584	2734	2925	3101	3269	3578	96
114_ 70.	8m	human.			1	1			2879	3045	3257	3455	3643	3991	101
120 78.					The second			STATE OF	3191	3374	3611	3829	4037	4420	107
	.03	10000	1	1	100	A .	8 4	1.00	3861	4082	4368	4631	4882	5350	117
144 113		1	1		1800			200	4596	4859	5200	5515	5811	6367	128

DIAM.	AREA						HEIGH	HT OF C	HIMNEY							EQUI
	(A)	50"	60'	70'	80'	90'	100'	110'	125'	150'	175'	200'	225'	250'	300'	Sq. Ch
Inches.	Sq. Ft.			Hors	e Power	= 6.5	AVH. W	hen 2 lbs	coal be	urned per	hour =	= 1 H. P.		200	1 000	Side of
18	1.77	84	92	98	104				1000		1		1000		I	
21	2.41	110	124	130	136			200	1000	-	-		t		-	16
24	3.14	144	156	170	182	196	- VE 100		10000		10530		2000 23			19
27	3.98	182	202	214	228	248	1 2000									22 24
20_	4.91	228	248	266	286	306	318									
33	5.94		298	326	344	364	384	404				+		-		27
36	7.07		358	384	410	436	456	482	514	1	E ST	1000	100		100000	30
39	8.30			448	482	514	540	566	604							32 35
42_	9.62			526	564	592	624	662	702	780						-
48	12.57		100000		728	774	820	858	916	1020		1000				38
54	15.90		ALTES E			982	1034	1086	1158	1294	1366	1000	FARITA S			43
60	19.64					1210	1274	1338	1430	1594	1690					48 54
66_	23.76						1548	1618	1730	1930	2042	2184				59
72	28.27	5000					1840	1924	2102	2294	2430	2600	2756			64
78	33.18				and the		100	2232	2412	2698	2918	3048	3238	3412		70
84	38.48							2320	2802	3126	3308	3536	3750	3952	4330	75
90_	.44.18								3218	3588	3796	4062	4310	4538	4972	80
96	50.27								3860	4082	4322	4622	4902	5168	5662	86
102	56.75		19.00					A 15 A	4134	4608	4858	5214	5532	5830	6390	91
108	63.62								4628	5168	5468	5850	6202	6538	7156	95
114	70.88									5758	6090	6514	6910	7286	7982	_101
	78.54		State of			1250			BOH BY	6382	6748	7222	7658	8074	8840	107
132	95.03	-	1000	5515	SHE R	6133	-			7722	8164	8736	9262	9764	10700	117
177	113.10		NO.							9192	9718	10400	11030	11622	12734	128
			REE						1200							

TABLE No. 10.

DIAM.	AREA					h	EIGHT	OF CHI	MNEY.							2000
	(A)	50'	60'	70'	80'	90'	100'	110'	125'	150'	175'	200	225'	250'	300'	EQUI
Inches.	8q. Ft.		1997		Pou	nds of	coal bur	ned per		= 13 x (The state of		1220	200	1 000	Side of
18		169	182	195	208			The same								
21	2.41	221	247	260	273			+		+						16
24	3.14	286	312	338	364	390		No.	BE				CERTIFICATION OF THE PERSON OF		123	19
27	3.98	364	403	429	455		17.154	THE REAL PROPERTY.							1	22
	0.00	304	403	429	433	494				7			142			24
30	4.91_	_455	494	533	572	611	637			100	1000	1000			10000	
33	5.94		598	650	689	728	767	806						+	+	27
36	7.07		715	767	819	871	910	962	1027	1000		1	1000			30
39	8.30	1000		897	962	1027	1079	1131	1209	1000	To all the	1000	1000		10000	32
							1010	1101	1203	1			100			35
42	9.62_		-	_1053	1128	1183	1248	1326	1404	1560	THE REAL PROPERTY.	E 100	1	10000	The state of	38
48	12.57				1458	1547	1638	1716	1833	2041		-				43
54	15.90					1963	2067	2171	2314	2587	2730	THE			1000	48
60	19.64					2418	2548	2678	2860	3198	3380					54
66	_23.76	diameter.					3094	3237	3458		-	0000	1030			
72	28.27	BENNE				-	3679	3848	4121	3861	4082	4368	-			59
78	33.18						3013	4524	4823	4589	4859	5200	5512	-		64
84	38.48			100				5239	5603	5395	5837	6097	6474	6825	1	70
								0239	3003	6253	6617	7072	7501	7904	8658	75
90	_44.18					100.00	4-2		6435	7176	7592	8125	8619	9074	9945	80
96	50.27		Single Property		E8183				7319	8164	8645	9243	9802	10335	11323	86
102 108	56.75					1	1000	100	8238	9217	9737	10425	11063	11661	12779	91
108	63.62	- 1		100	2803	SAE.		1000	9256	10335		11700	12402	13078	14313	96
114	70.88	1000	-	1	23/23	TO SE				10000		.,,	12102	10010	17010	30
120							-	-		11518	12181	13026	13819	14573	15084	101
132	78.54 95.03			10000	-598	THE REAL PROPERTY.	1835	25.00	THE PARTY OF	12766	13494			16146		107
144	113.10		- 5 3			203	100		7-7-1-5	15444	16328		18525		21398	117
	110.10	2000		1213		13000	100		NELSO.	18382	19435			23244	25467	128
															20,01	12

This table has been calculated by D. K. Clark's rules.

1	'A	BI	E	N	0.	12

Height.	Diameter of Flue.	Top sectional a	rea of flue in feet.	Coal per hour.	Area of grate.
Feet,	Inches.	Area.	Per lb, coal per hour.	Pounds.	Square feet.
40	16	1.39	1.41	142	9.5
45	18	1.77	1.34	190	12 7
50	20	2.19	1.27	248	16.5
55	22	2.63	1.21	314	20.9
60	24	3.14	1.16	390	26.0
65	26	3.69	1.11	477	31.7
70	28	4.26	1.07	574	38 3
75	30	4.91	1.04	682	45.5
80	32	5.60	1.00	801	53 4
85	34	6 29	.97	932	62.1
90	36	7.09	.95	1076	71.7
95	38	7.89	.92	1231	82.1
100	40	8.71	.90	1394	93.0
105	42	9.62	.88	1582	105.5
110	44	10.57	.86	1777	118.4
115	46	11.52	.84	1985	132.3
120	48	12.86	.82	2208	147.2
125	50	13 65	80	2446 -	163.1
130	52	14.73	.79	2698	179.8
135	54	15 90	.77	2964	197.6
140	56	17.12	.76	3247	216.4
145	58	18.32	.74	3544	236.2
150	60	19.63	.73	3858	257.2
155	62	20.99	.72	4187	279.1
160	64	22.31	.71	4533	302.2
165	66	23.76	.70	4896	326.4
170	68	25.24	.69	5275	351.6
175	70	26.69	.68	5672	378 1
180	72	28.27	.67	6086	405.7
185	74	29.90	.66	6517	434 5
190	76	31.47	.65	6967	464.5
195	78	33.18	.64	7434	495.6
200	80	34.94	.63	7920	526.6

RATE OF COMBUSTION DUE TO HEIGHT OF CHIMNEY.

Trowbridge's "Heat and Heat Engines" gives the following table showing the heights of chimneys for producing certain rates of combustion per square foot of section of the chimney-flue. It is best adapted to chimneys where a good grade of large-sized anthracite coal is used.

175 200' 225' 250'	ERS.	S. per hour.)				18878 21580 22750 25008 26847	28730 80247 82673 84450 86877 88871 41840 48598	46068 48910 51047 53820 61750 65087 73537 77480
200′ 226′	ERS.	nour.)				AND A COMPANY OF THE PARK OF T		
200′ 226′	ERS.	nour.)				AND A COMPANY OF THE PARK OF T		
200′ 226′	ERS.	nour.)				AND A COMPANY OF THE PARK OF T	28730 82673 86877 41840	1047 11047 11750
2000	ERS.	nour.)				18878 21580 25008	2873(3267) 36877 4134(1606 51047 3175 3175
2000	ERS.	nour.)				183 215 250	287 826 368 413	160 317 317
2000	ERS.	nour.)				222	98894	#1000
2000	grs.	nour.)		1111				A ST OF L
	grs.	nour.)		1111				
	grs.	nour.)				14562 17888 20328 28578	27083 30810 34753 39000	48148 48148 58240
	grs.	nour.)		THE REAL PROPERTY AND PERSONS ASSESSED.		10 20 20 10	0820	4153
	EBS.	nour.)				2221	88888	4450
175/	ERS.	nou					> > > 00	~~~
175	ERS.				9100	18607 16197 19457 22057	25807 28817 32457 86448	40603 44980 54427
17.0	ERS				63	92.400	88844	8644
	68	190			::37	3223	20000	4400
-	3	-			• •			
ALC: U	1 =				5200 6803 8623 0660	97	57	38898 42558 51480
8	m	H			8888	8228	82224	8884
15	Z	7.			2002	2112	0,0000	30 4 10 0
0.34	153	5	*					
550	0	0	* *	308	381188	4-10010	5000	
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	NG	In		100	0,0000	6233	1:1:	2.1
6	H	-86		828	88	2500		
F	EA	Jer.			To de de la			
	H	I		-1 co -1 co	0000	0000		
	ER	308		8000	9366	31		
8	B	J.		20000	4500	000	1 1 1 1 1	
-	A	100	1 : : : :					
-		100	40.	2-1-0000	0000			2011
1		8.	04	5000	46 45 96			
8	100	18	128	8 8 8 8 8	80000			
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		1088	173	0000	920			
80		188	0 6 6 1	222	84			
		16						
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	2 .		7.688		12.0		1000	95.8
8				4101-00		88888	4000	- 00
7700	a 50 60 70 80 90 100 110 125 150	60' 70' 80' 90' 100' 110' 125' WATER-HEATING SURFACE	50' 60' 70' 80' 90'	60' 60' 70' 80' 90' (0.81b) 7 568 607 650 698 4 968 1040 1127 1218 1800 8 1218 1843 1480 1517 1647 1647	50 60 70 80 90 7 563 607 650 693 8 1218 1845 1430 1517 1647 1 1517 1647 1777 1907 2087 4 968 1040 1127 1218 1800 8 1218 1843 1430 1517 1647 1 1517 1647 1777 1907 2087 4 2388 2557 2397 2427 7 2388 2557 2780 2908 990 3207 3428	567 607 707 807 907 10.8 lb 10.8	1 1517 1647 177 1907 2008 170 18	1 1 1 1 1 1 1 1 1 1

TABLE No. 13.

Height of chimney in feet.	burned per hour per square foot of section	Lbs. of coal burned per square foot of grate, the iatio of grate area to chimney flue area being 8 to 1.	Height of chimney in feet.	Lbs. of coal burned per hour per square	Lbs. of coal burned per square foot of grate, the ratio of grate area to chimney flue area being 8 to 1.
20 25 30 35 40 45 50 55 60 65	60 68 76 84 93 99 105 111 116	7.5 8.5 9.5 10.5 11.6 12.4 13.1 13.8 14.5	70 75 80 85 90 95 100 105 110	126 131 135 139 144 148 152 156 160	15.8 16.4 16.9 17.4 18.0 18.5 19.0 19.5 20.0

Dr. R. H. Thurston's rule for the rate of combustion for a given height of chimney (Trans. A. S. M. E., vol. xi., p. 991) is: Subtract one from twice the square root of the height, and the result is the rate of combustion in pounds per square foot of grate per hour, for anthracite coal; or rate $= 2\sqrt{H} - 1$, in which H is the height of chimney in feet.

This rule gives the following table:

The results agree closely with Trowbridge's table given above. In practice, however, the high rates of combustion for high chimneys given by the formulæ are seldom obtained, for the reason that with high chimneys there are long horizontal flues, serving many boilers, and the friction and interference of the currents of gases from the different boilers diminish the intensity of the draft at the boiler from what it was at the chimney.

In a battery of several boilers connected to a chimney 150 feet in height there has been found \(\frac{3}{4} \) inch of water draft at the boiler nearest the chimney, and only \(\frac{1}{4} \) inch at the boiler farthest from it.

The first boiler was wasting fuel from an excessive temperature of the chimney gases, 900° Fahr., having too large a

grate surface for the draft, and the last boiler was working below its capacity, and with poor economy, on account of poor draft.

Theron Skeel gives the following relative amounts of coal that can be burned in the same time with chimneys of various heights:

J. J. DeKinder finds the best results to be obtained by using chimneys of the following heights:

75 feet for free-burning bituminous coal.

100 feet for free-burning bituminous slack.

115 feet for slow-burning bituminous coal.

125 feet for anthracite pea coal.

150 feet for anthracite buckwheat coal.

with a draft for anthracite coal of 0.75 to 0.88 inch of water.

This agrees with the conclusions of Emery and Hague.

AIR-SPACE IN GRATES.

The successful performance of a chimney depends upon very many local conditions, among which, and very important, is the amount of air supplied to the burning fuel and allowed to pass through it.

The following list gives the proper size of air-space and thickness of metal in the bar for different fuels.

4-inch opening and 3-inch iron for screenings.

3/s-inch opening and 3/s-inch iron for buckwheat coal.

12-inch opening and 12-inch iron for nut or pea coal.

5-inch opening and 1-inch iron for stove coal.

3-inch opening and 1-inch iron for egg coal.

3-inch opening and 1-inch iron for broken coal.

1-inch opening and 1-inch iron for lump coal.

4-inch opening and 3-inch iron for sawdust.

3-inch opening and 3-inch iron for sawdust.

1-inch opening and 1-inch iron for shavings.

5-inch opening and 1-inch iron for shavings.

For bituminous coal, 5 or 3-inch opening and 1-inch iron.

VOLUME OF AIR PASSING THROUGH CHIMNEY.

According to Professor H. B. Gale, the velocity for maximum draft in chimneys is between six and fourteen feet per second, depending on the height of the chimney and temperature of the escaping gases; in brick-stacks it sometimes is as low a rate as three feet per second. The exact rate at which the best draft is produced depends on so many variables, such as flue temperatures, grate air-space, kind of conditions of fuel, etc., that it is probably not the same in any two chimneys or power plants.

VELOCITY OF GASES.

Lang recommends "for velocity of chimney gases, V_n , 13.12 feet per second; in sheltered locations 9.84 feet per second.

If prevailing winds come over steep mountains and fall on the top of the chimney, then V_n must be correspondingly increased from 19.68 to 22.96 feet per second; or the top of the chimney must be provided with proper covers for such unfavorable directions (wind caps, etc.).

With good wind caps V_n may be reduced from 4.92 to 5.65 feet a second.

Wind caps, on account of their dangerous position, are only recommended in exceptional cases.

If a number of boiler-furnaces discharge their gases in one and the same chimney, then V_n must be increased for the full working number, so that in case there are less than the whole number of boilers under fire a sufficient exhaust velocity of the gases will still be obtained. In place of the average value of $V_n = 13.12$ feet per second; the following values may be substituted:

For 3 boilers, $V_n = 16.40$ ft. per sec. = 984.0 ft. per minute.

" 7 " $V_n = 19.68$ " " = 1180.8 " " 12 " $V_n = 22.96$ " " = 1377.6 "

" more, 12 + X boilers, $V_n = 22.96 + \frac{X \times 3.28}{20}$ ft. a second.



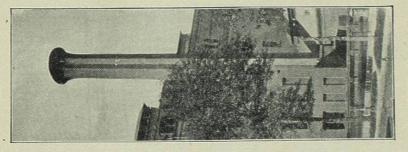
WIND-PRESSURE.

The scale of the Smithsonian Institution at Washington for the estimation and description of the velocity and pressure of the wind, calculated by Smeaton's Rule, is as follows:

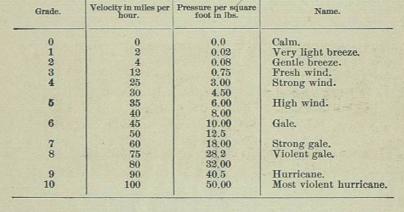
Divide the square of the velocity in miles per hour by 200; the quotient is the pressure in pounds per square foot.

TABLE No. 14. CHESTON DXAE4

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ILLUS. No. 2. THREE BRICK CHIMNEYS.

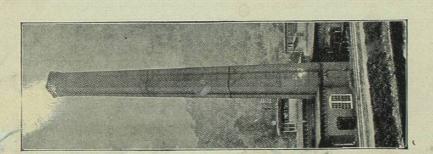


In the United States the general practice is to assume fifty pounds wind-pressure per square foot as the highest to be considered.

No record of such a high pressure has been heard of, or is likely to be, except in the extreme hurricane, with cyclonic conditions present, as in the East St. Louis, Mo., tornado of 1896, when the brick chimney of the Electric Light Station was partially destroyed and blown down.

From calculations made since the occurrence, the force of the wind must have been about ninety pounds per square foot.

During the Galveston, Tex., tornado of September, 1900, the barometer dropped to 27.3 inches, and the velocity of the wind was reported by a United States Engineer to have been as high as 100 miles per hour.



The *Engineer*, London, says: the pressure of the wind on plane surfaces has been found by experiments to be approximately:

 $q=rac{v^2}{430}\cos i$.

v = velocity of wind in feet per second.

i =angle between the normal to the plane and the direction of the wind.

q =pressure in pounds per square foot of plane.

The above, of course, does not apply to curved surfaces.

CHAPTER V

FOUNDATION MATERIALS. BRICK CHIMNEY MATERIALS

LOGICALLY and from an engineering stand-point, the first detail of chimney construction is the foundation.

Before considering this topic, a brief statement of the qualities and strengths of various soils, with reference to their ability to support foundations, is requisite.

BEARING FOWER OF SOILS.

The building laws of New York City allow 4 tons per square foot as a safe load for "good solid natural earth."

The laws of Chicago specify 13 tons for pure clay, fifteen feet or more thick; 2 tons for pure dry sand, fifteen feet or more thick; and 1½ tons for a mixture of clay and sand of the same depth.

Ordinary practice gives the following:

200 tons per square foot for solid bed rock.

5 to 25 tons per square foot for rock broken, but well compacted.

4 tons per square foot for pure clay fifteen feet or more thick.

1 ton per square foot for soft wet clay.

8 tons per square foot for gravel well packed and confined.

4 tons per square foot for pure dry sand well packed and confined.

2 tons per square foot for pure dry sand in its natural bed.

½ ton per square foot for quicksands and marshy soils.

PILING.

Piling must be resorted to when the soil is very sandy or loose.