Observaciones de los pares de estrellas-Continuación.

ABRIL 25 DE 1893.

	Cronómetro.	Micró-	Niv	rel.		δ		1//	2	+ 8')			Correccio	nes.		Latitu
Pares.	Cronometro.	metro.	oc.	ob.		0		72 (0 7	-0)		m n 5 32.12 - 0.55 0.09 0.00 6 7.96 0.00 0.10 ρ.00	31° 20			
					0	,	"	0	,	"	,	"				"
10'		44.242	4.0	35.7	31	13	55.25								1178	
		53.717	2.7	34.3	31	15	12.20	31	14	33.72	+ 5	32.12	- 0.55	0.09	0.00	5.3
11'		44.1965	8.4	40.3	29	15	13.06									
		54.6940	8.4	40.3	33	12	42.44	31	13	57.75	+6	7,96	0.00	0.10	0.00	5.8
12'		55,901	7.9	39.6	20	47	32.58								P. C.	
		43.608	6.1	38.0	42	6	59.34	31	27	15.96	- 7	10.90	- 0.85	- 0.13	0.00	4.0
13'		56,801	7.5	39.4	36	0	35.81									
-		42,410	8.8	40.7	26		50.27	91	11	43.04	18	24.79	- 0.65	0.14	0.00	7.3
		2.110	0.0	20.1			00.01	01	**	29.01	100		3.00	3.11	0.00	1.0
14'		43.9695	8.4	40.3	23	47	22.72				189					
287		54.3510	8.5	40.6	38	40	40.42	31	14	1.57	+ 6	3.89	0.10	0.10	0.00	5.

Discusión.

Pares.	Estrellas.	Latitud 31° 20′	Promedio.	Δ	∇_3	Δφ	Δ φ 2	η
1	Safford 8 A	6.19	6.19			0.88	0.7744	1.000
	" 13 A							
2 .	New 582	4.35	5.28	0.93	0.8649	0.03	0.0009	0.333
	Safford 28 B	5 56		0.28	0.0784			
		5.92		0.64	0.4096			
4	Safford 91 A	6.56	6.14	0.08	0.0064	0.83	0,6889	0.333
	" 104 C	6.22		0.49	0.2401			
		5.65		0.49	0.2401			
5	8 Draconis A	6.55	5.39	1.16	1.3456	0.08	0.0064	0.333
	New 597	5.01		0.38	0.1444			
		4.60		0.79	0.6241			
6	Safford 127 A	6.79	6.96	0.17	0.0289	1.65	2.7225	0.333
	" 184 B	7.20		0.24	0.0576			
		6.89		0.07	0.0049			
7	Safford 142 B	6.97	6.61	0.36	0.1296	1.30	1.6900	0.500
	" 152 B	6,25		0.36	0.1296			
9	Safford 157 A	4.16	5.09	0.93	0.8649	0.22	0.0484	0.500
	" 170 A	6.02		0.93	0.8649			
10	Safford 178 B	4.87	5.06	0.19	0.0361	0.25	0.0625	0.338
	" 175 A	5.50		0.44	0.1936			
		4.80		0.26	0.0676			
11	Safford 188 A	4.10	4.09	0.01	0.0001	1.22	1.4884	0.333
	,, 195 C	4.34		0.25	0.0625			
		3.82		0.27	0.0729			
12	Safford 221 A	5,03	5.70	0.67	0.4489	0.39	0.1521	0.333
	,, 232 A	6.70		1.00	1.0000			
		5.37		0.33	0.1089	The state of the s	1	

Discusión-Continuación.

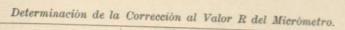
Pares Estrellas Latitude Promedio A			1	iscusion-	Continua	cion.			
### Safford 224 A.	Pa		31° 20′	Promedio	Δ	Δ2	Δφ	Δ φ2	η.
### Safford 254 A. 8.10 0.82 0.7204 6.73 0.85 0.7225 8.10 0.85 0.7225 8.10 0.85 0.7225 8.10 0.85 0.7225 8.10 0.85 0.7225 8.10 0.85 0.8136 8.10 0.85 0.8136 8.10 0.85 0.8136 8.10 0.85 0.8136 8.10 0.85 0.8136 8.10 0.85 0.8136 8.10 0.85 0.8136 8.10 0.85 0.8136 8.10 0.85 0.825 8.10 0.85 0.825 8.10 0.85 0.825 8.10 0.85 0.825 8.10 0.85 0.825 8.10 0.85 0.825 8.10 0.85 0.825 8.10 0.85 0.825 8.10 0.85 0.825 8.10 0.85 0.825 8.10 0.85 0.825 8.10 0.85 0.825 8.10 0.85 0.825 8.10 0.85 0.825 8.10 0.85 0.825 8.10 0.85 0.825 8.10 0.85 0.85 8.10	1			7.58	0.34	0.1156	2.27	5.1529	0.999
### Safford 254 A. 5.29		" 252 A	8.10		0.52	0.2704		-	0 333
3.65 0.54 0.5916 3.63 0.54 0.5916 3.63 0.56 0.3136 b Safford 202 B.			6.73		0.85	0.7225			
b Safford 2022 B 4.65 0.56 0.56 0.3136 0.02 0.0004 0.500 c 274 A 5.94 4.65 0.65 0.42159 0.70 0.4900 0.333 c Safford 2022 B 5.84 4.61 1.23 1.1519 0.70 0.4900 0.333 d Safford 310 B 3.41 0.02 0.0004 1.90 3.4100 0.33 d Safford 315 A 7.75 0.33 0.1225 0.300 0.333 d Safford 315 A 7.15 6.43 0.72 0.3184 1.12 1.2544 0.500 f Safford 328 C 4.00 3.51 0.49 0.301 1.89 3.2600 0.333 g Safford 343 C 3.76 3.78 0.02 0.0004 1.53 2.3400 0.500 g Safford 365 C 4.00 0.01 0.0001 1.53 2.3400 0.500 g Safford 376 C	1. (Safford 254 A	5.29	4.19	1.10	1.2100	1 10	1000	
b Safford 262 B 4.63 5.29 0.64 0.406 0.02 0.004 0.500 c Safford 262 B 5.84 4.61 1.23 1.5199 0.70 0.4900 0.333 d Safford 302 B 5.84 4.61 1.23 1.5199 0.70 0.4900 0.333 d Safford 310 B 3.43 3.41 0.02 0.0004 1.90 3.6100 0.333 a 311 B 3.76 0.37 0.1369 1.12 1.2544 0.200 d Safford 315 A 7.15 6.43 0.72 0.3184 1.12 1.2544 0.200 f Safford 328 C 4.00 3.51 0.49 0.3401 1.80 3.2400 0.333 g Safford 343 C 3.76 3.78 0.02 0.004 1.53 2.3600 0.353 g Safford 376 C 5.89 5.92 0.01 0.0001 0.61 0.3721 0.333 d <td></td> <td></td> <td>3.65</td> <td></td> <td>0.54</td> <td></td> <td>1.10</td> <td>1.3044</td> <td>0.333</td>			3.65		0.54		1.10	1.3044	0.333
c Safford 292 B. 5.84			3.63		0.56				
c Safford 292 B. 5.84	7	Safford 262 B	4.63	5.99	0.84	0.4000			
c Safford 529 B. 5.84 4.61 1.23 1.5129 0.70 0.4900 0.333 4.19 0.80 0.42 0.1394 d.19 0.42 0.1394 d.19 0.42 0.1394 d.19 0.42 0.1394 d.19 0.35 0.1225 0.1394 d.19 0.35 0.1225 0.1399 d.190 0.333 0.34 0.37 0.1309 d.190 0.333 0.332 d.190 0.37 0.1309 d.190 0.333 0.332 d.190 0.333 0.332 d.190 0.333 0.332 d.190 0.333 0.332 d.190 0.3401 1.80 0.324 0.333 0.322 0.1764 d.190 0.333 0.322 0.334 d.190 0.333 0.333 0.366 0.36 0.36 0.36 0.36							0.02	0.0004	0.500
## Safford 316 B. 3.81					0.00	0.4223		1	
### Safford 310 B. 3.43 3.41 0.02 0.0004 1.90 3.6100 0.333 ### Safford 315 A. 7.15 6.43 0.72 0.5184 1.12 1.2544 0.500 ### Safford 328 C. 4.00 3.51 0.49 0.2401 1.80 3.2400 0.333 ### Safford 328 C. 4.00 3.51 0.49 0.2401 1.80 3.2400 0.333 ### Safford 328 C. 4.00 3.51 0.49 0.2401 1.80 3.2400 0.333 ### Safford 328 C. 3.76 3.78 0.02 0.0004 1.53 2.3409 0.500 ### Safford 336 C. 3.76 3.78 0.02 0.0004 1.53 2.3409 0.500 ### Safford 376 C. 5.89 5.92 0.03 0.0009 0.61 0.3721 0.333 ### Safford 386 A. 3.87 3.92 0.06 0.0025 1.39 1.9221 0.333 ### Safford 386 A. 3.87 3.92 0.06 0.0025 1.39 1.9221 0.333 ### Safford 430 B. 4.16 4.47 0.31 0.0661 0.84 0.7056 0.333 ### Safford 430 B. 4.16 4.47 0.31 0.0661 0.84 0.7056 0.333 ### Safford 441 A. 5.77 4.62 1.15 1.3225 0.69 0.4761 0.333 ### Safford 400 A. 4.34 0.28 0.0784 0.22 0.1024 ### Safford 400 A. 4.65 4.60 0.05 0.0025 0.71 0.5041 0.333 ### Safford 400 A. 4.65 4.60 0.05 0.0025 0.71 0.5041 0.333 ### Safford 501 B. 7.05 6.53 0.52 0.2704 1.22 1.4884 0.500 ### Safford 505 B. 7.05 6.53 0.52 0.2704 1.22 1.4884 0.500 ### Safford 505 B. 5.23 4.25 0.98 0.9004 1.06 1.1295 0.333 ### Safford 505 B. 5.23 4.25 0.98 0.9004 1.06 1.1295 0.333 ### Safford 505 B. 5.23 4.25 0.98 0.9004 1.06 1.1295 0.333 ### Safford 505 B. 5.23 4.25 0.98 0.9004 1.06 1.1295 0.333 ### Safford 505 B. 5.23 4.25 0.98 0.9004 1.06 1.1295 0.333 ### Safford 505 B. 5.23 4.25 0.98 0.9004 1.06 1.05 1.1295 0.333 ### Safford 505 B. 5.23 4.25 0.98 0.9004 1.06 1.05 1.1295 0.333 ### Safford 505 B. 5.23 4.25 0.98 0.9004 1.06 1.06 1.1295 0.333 ### Safford 505 B. 5.23 4.25 0.98 0.9004 1.06 1.06 1.1295 0.333 ### Saff				4.61	1.23	1.5129	0.70	0.4900	0.333
d Safford 310 B. 3.43 3.41 0.02 0.0004 1.90 3.6100 0.333 e Safford 315 A. 7.15 6.43 0.72 0.5184 1.12 1.2544 0.500 f Safford 325 C. 5.70 0.73 0.523 0.529 1.12 1.2544 0.500 f Safford 325 C. 4.00 3.51 0.49 0.2401 1.80 3.2400 0.333 g Safford 325 C. 4.00 3.51 0.49 0.2401 1.80 3.2400 0.333 g Safford 343 C. 3.78 0.02 0.0004 1.53 2.3409 0.500 g Safford 343 C. 3.78 0.02 0.0004 1.53 2.3409 0.500 h Safford 356 B. 3.79 0.01 0.0001 1.53 2.3409 0.500 h Safford 366 A. 3.87 3.92 0.03 0.0009 0.61 0.3721 0.333 d Safford 386 A. 3.87 3.92 0.06 0.0025 1.39 1.9321 0.333		11 001 D				0.6400		1	
## Safford 343 C.			4.19		0.42	0.1264			
## Safford 315 A.	d	Safford 310 B	3.43	3.41	0.02	0.0004	1.90	3,6100	0.888
## Safford 315 A. 7.15 6.43 0.72 0.5184 1.12 1.2544 0.500 ## Safford 328 C. 5.70 0.73 0.329 0.329 ## Safford 328 C. 4.00 3.51 0.49 0.2401 1.80 3.2400 0.333 ## Safford 328 C. 4.00 3.51 0.49 0.2401 1.80 3.2400 0.333 ## Safford 328 C. 3.76 3.78 0.07 0.0049 0.1764 ## Safford 343 C. 3.76 3.78 0.02 0.0004 1.53 2.8409 0.500 ## Safford 343 C. 5.89 5.92 0.03 0.0009 0.61 0.3721 0.333 ## Safford 376 C. 5.89 5.92 0.03 0.0009 0.61 0.3721 0.333 ## Safford 385 A. 3.87 3.92 0.06 0.0025 1.39 1.9321 0.333 ## Safford 385 A. 3.87 3.92 0.06 0.0025 1.39 1.9321 0.333 ## Safford 430 B. 4.16 4.47 0.31 0.0961 0.84 0.7056 0.333 ## Safford 441 A. 5.77 4.62 1.15 1.3225 0.69 0.4761 0.333 ## Safford 441 A. 5.77 4.62 1.15 1.3225 0.69 0.4761 0.333 ## Safford 441 A. 5.77 4.62 1.15 1.3225 0.69 0.4761 0.333 ## Safford 440 A. 4.45 0.28 0.0784 0.000 ## Safford 450 B. 7.05 6.53 0.32 0.2704 1.22 1.4884 0.500 ## Safford 301 B. 7.05 6.53 0.32 0.2704 1.22 1.4884 0.500 ## Safford 325 A. 6.57 6.81 0.24 0.576 1.50 2.2200 0.333 ## Safford 325 A. 6.57 0.24 0.6576 0.48 0.2904 ## Safford 356 B. 5.23 4.25 0.98 0.9004 1.06 1.1236 0.833.		" 311 B	3.76		0.85	0.1225			7.00
## Safford 385 C. 5.70 0.73 0.5389 1.12 1.2044 0.500 ## Safford 385 C. 4.00 3.51 0.49 0.2401 1.80 3.2400 0.333 ## Safford 343 C. 3.76 3.78 0.02 0.0004 1.53 2.3409 0.500 ## Safford 376 C. 5.89 5.92 0.03 0.0009 0.61 0.3721 0.333 ## Safford 376 C. 5.89 5.92 0.03 0.0009 0.61 0.3721 0.333 ## Safford 386 A. 3.87 3.92 0.05 0.0025 1.39 1.9321 0.333 ## Safford 430 B. 4.16 4.47 0.31 0.0961 0.84 0.7056 0.333 ## Safford 441 A. 5.77 4.62 1.15 1.3225 0.69 0.4761 0.333 ## Safford 441 A. 5.77 4.62 1.15 1.3225 0.69 0.4761 0.333 ## Safford 440 A. 4.34 0.28 0.0784 0.7744 ## Safford 490 A. 4.65 4.60 0.05 0.0025 0.774 0.5041 0.333 ## Safford 490 A. 4.65 4.60 0.05 0.0025 0.774 0.5041 0.333 ## Safford 501 B. 7.05 6.53 0.52 0.2704 1.22 1.4884 0.500 ## Safford 525 A. 6.57 6.81 0.24 0.576 1.50 2.2500 0.333 ## Safford 536 B. 5.23 4.25 0.98 0.9004 1.06 1.1296 0.333 ## Safford 536 B. 5.23 4.25 0.98 0.9004 1.06 1.1296 0.333 ## Safford 536 B. 5.23 4.25 0.98 0.9004 1.06 1.1296 0.333			3.04		0.37	0.1369			
## Safford 328 C. 5.70 0.73 0.5329 ## Safford 328 C. 4.00 3.51 0.49 0.2401 1.80 3.2400 0.333 ## Safford 343 C. 3.76 3.78 0.02 0.0004 1.53 2.3400 0.500 ## Safford 376 C. 5.89 5.92 0.03 0.0009 0.61 0.3721 0.333 ## Safford 376 C. 5.89 5.92 0.03 0.0009 0.61 0.3721 0.333 ## Safford 386 A. 3.87 3.92 0.05 0.025 1.39 1.3921 0.333 ## Safford 386 A. 3.87 3.92 0.05 0.0025 1.39 1.3921 0.333 ## Safford 430 B. 4.16 4.47 0.31 0.0661 0.84 0.7056 0.333 ## Safford 441 A. 5.77 4.62 1.15 1.3225 0.69 0.4761 0.333 ## Safford 441 A. 5.77 4.62 1.15 1.3225 0.69 0.4761 0.333 ## Safford 440 A. 4.34 0.28 0.0784 ## Safford 490 A. 4.65 4.60 0.05 0.0025 0.71 0.5041 0.333 ## Safford 501 B. 7.05 6.53 0.52 0.2704 1.22 1.4884 0.500 ## Safford 525 A. 6.57 6.81 0.24 0.576 1.50 2.2500 0.333 ## Safford 525 B. 5.23 4.25 0.98 0.9604 1.06 1.1296 0.333 ## Safford 536 B. 5.23 4.25 0.98 0.9604 1.06 1.1296 0.333 ## Safford 536 B. 5.23 4.25 0.98 0.9604 1.06 1.1296 0.333 ## Safford 536 B. 5.23 4.25 0.98 0.9604 1.06 1.1296 0.333		Safford 315 A	7.15	6,43	0.72	0.5184	1 10		
f Safford 328 C. 4.00 3.51 0.49 0.2401 1.80 3.2400 0.333 g Safford 343 C. 3.76 3.78 0.02 0.0004 1.53 2.3409 0.500 h Safford 376 C. 5.89 5.92 0.03 0.0009 0.61 0.3721 0.333 h Safford 376 C. 5.89 5.92 0.03 0.0009 0.61 0.3721 0.333 h Safford 386 A. 3.87 3.92 0.05 0.025 1.39 1.9321 0.333 i Safford 430 B. 4.16 4.47 0.31 0.0961 0.84 0.7056 0.333 m Safford 441 A. 5.77 4.62 1.15 1.3225 0.69 0.4761 0.333 m Safford 490 A. 4.63 4.60 0.03 0.0025 0.71 0.5041 0.333 m Safford 490 A. 4.65 4.60 0.05 0.0025 0.71 0.5041 0.333 m Safford 501 B. 7.05 6.53 0.52 0.2704 <td></td> <td>,, 325 C</td> <td>5.70</td> <td></td> <td></td> <td></td> <td>1.12</td> <td>1,4544</td> <td>0,500</td>		,, 325 C	5.70				1.12	1,4544	0,500
9 Safford 343 C. 3.76 3.78 0.02 0.0004 1.53 2.3409 0.500 h Safford 376 C. 5.89 5.92 0.03 0.0009 0.61 0.3721 0.333 " 380 B. 6.06 0.14 0.0196 0.14 0.0196 5.80 0.12 0.014 0.0196 i Safford 388 A. 3.87 3.92 0.05 0.065 0.065 1.39 1.9321 0.333 " 402 A. 4.23 0.31 0.0661 j Safford 430 B. 4.16 4.47 0.31 0.0661 0.84 0.7056 0.333 " 439 A. 4.79 0.32 0.1024 0.0004 M Safford 441 A. 5.77 4.62 1.15 1.3225 0.69 0.4761 0.333 " 400 A. 4.34 0.88 0.7744 1' Safford 490 A. 4.65 4.60 0.03 0.0025 0.71 0.5041 0.333 1' Safford 501 B. 7.05 6.53 0.52 0.2704 1.22 1.4884 0.500 0.52 0.2704 2' Safford 501 B. 7.05 6.53 0.52 0.2704 1.22 1.4884 0.500 0.52 0.2704 3' Safford 355 B. 5.23 4.25 0.98 0.9004 1.06 1.1236 0.333 0.333 0.32 0.3204 4' Safford 556 B. 5.23 4.25 0.98 0.9004 1.06 1.1236 0.333 0.333 0.32 0.3204		Safford 398 C	4.00	0.71					
9 Safford 343 C. 3.76 3.78 0.02 0.0004 1.53 2.3409 0.500 h Safford 376 C. 5.89 5.92 0.03 0.0009 0.61 0.3721 0.333 " 380 B. 6.06 0.14 0.0196 5.80 0.12 0.0144 i Safford 386 A. 3.87 3.92 0.05 0.0025 1.39 1.9321 0.333 " 402 A. 4.23 0.31 0.0061 J Safford 430 B. 4.16 4.47 0.31 0.0061 0.84 0.7086 0.333 " 439 A. 4.79 0.32 0.1024 4.45 0.02 0.002 0.0004 M Safford 441 A. 5.77 4.62 1.15 1.3225 0.69 0.4761 0.333 " 400 A. 4.34 0.28 0.0784 3.74 0.88 0.7744 1' Safford 490 A. 4.65 4.60 0.03 0.0025 0.71 0.5041 0.333 " 435 A. 4.70 0.10 0.000 0.000 4.44 0.06 0.0036 2' Safford 501 B. 7.05 6.33 0.52 0.2704 1.22 1.4884 0.500 " 513 A. 6.01 0.52 0.2704 3' Safford 355 B. 5.23 4.25 0.98 0.9004 1.06 1.1236 0.333 4' Safford 556 B. 5.23 4.25 0.98 0.9004 1.06 1.1236 0.333 " 562 A. 3.94 0.31 0.0961		-		8.51			1.80	3.2400	0.333
9 Safford 343 C. 3.76 3.78 0.02 0.0004 1.53 2.3409 0.500 " 336 B. 3.79 0.01 0.0001 *** **Safford 376 C. 5.89 5.92 0.03 0.0009 0.61 0.3721 0.333 " 380 B. 6.06 0.14 0.0196 0.12 0.0144 *** **Safford 386 A. 3.87 3.92 0.05 0.0025 1.39 1.9321 0.333 " 402 A. 4.23 0.31 0.0961 **Safford 430 B. 4.16 4.47 0.31 0.0961 0.84 0.7056 0.333 " 439 A. 4.79 0.32 0.1024 4.45 0.002 0.0004 ***M** **Safford 441 A. 5.77 4.62 1.15 1.3225 0.69 0.4761 0.333 " 460 A. 4.34 0.28 0.0744 1' Safford 490 A. 4.65 4.60 0.05 0.0025 0.71 0.5041 0.333 " 495 A. 4.70 0.10 0.0100 0.444 2' Safford 501 B. 7.05 6.53 0.52 0.2704 1.22 1.4884 0.500 " 513 A. 6.01 0.52 0.320 0.3704 3' Safford 525 A. 6.57 6.81 0.24 0.576 1.50 2.2500 0.333 " 544 B. 6.57 0.24 0.0576 7 2.9 0.48 0.2304 4' Safford 556 B. 5.23 4.25 0.98 0.9904 1.06 1.1236 0.335 .									
## Safford 376 C 5.89 5.92 0.03 0.0009 0.61 0.3721 0.333 ## Safford 376 C 5.89 5.92 0.03 0.0009 0.61 0.3721 0.333 ## Safford 386 A 3.87 3.92 0.05 0.0025 1.39 1.9321 0.333 ## Safford 490 B. 4.16 4.47 0.31 0.0961 0.84 0.7066 0.333 ## Safford 490 B. 4.16 4.47 0.31 0.0961 0.84 0.7066 0.333 ## Safford 441 A. 5.77 4.62 1.15 1.3225 0.69 0.4761 0.333 ## Safford 490 A. 4.34 0.28 0.0784 3.74 0.88 0.7744 ## Safford 490 A. 4.65 4.60 0.05 0.0025 0.71 0.5041 0.333 ## Safford 501 B. 7.05 6.53 0.52 0.2704 1.22 1.4884 0.500 ## Safford 525 A. 6.57 6.81 0.24 0.576 1.50 2.2500 0.333 ## Safford 536 B. 5.23 4.25 0.98 0.9904 1.06 1.1236 0.335. ## Safford 536 B. 5.23 4.25 0.98 0.9904 1.06 1.1236 0.335. ## Safford 536 B. 5.23 4.25 0.98 0.9904 1.06 1.1236 0.335.					0.45	0.1764			
h Safford 376 C. 5.89 5.92 0.03 0.0009 0.61 0.3721 0.333 " 380 B. 6.06 0.14 0.0196 0.014 0.0196 0.0144 i Safford 386 A. 3.87 3.92 0.05 0.0025 1.39 1.9321 0.333 " 402 A. 4.23 0.31 0.0961 0.066 0.0676 ! Safford 430 B. 4.16 4.47 0.31 0.0961 0.84 0.7056 0.333 " 439 A. 4.79 0.32 0.1024 0.0004 0.0004 0.0004 " Safford 441 A. 5.77 4.62 1.15 1.3225 0.69 0.4761 0.333 " 460 A. 4.34 0.28 0.0784 0.0784 0.7744 1' Safford 490 A. 4.65 4.60 0.05 0.0025 0.71 0.5041 0.333 " 495 A. 4.70 0.10 0.0100 0.0005 0.0025 0.71 0.5041 0.333 2' Safford 525 A. </td <td>g</td> <td></td> <td></td> <td>3.78</td> <td>0.02</td> <td>0.0004</td> <td>1.58</td> <td>2.3409</td> <td>0.500</td>	g			3.78	0.02	0.0004	1.58	2.3409	0.500
## Safford 490 A.		" 356 B	3.79		0.01	0.0001		Contraction of the last	
## Safford 490 A. 4.65	h	Safford 376 C	5.89	5.92	0.03	0.0009	0.61	0.3721	0.833
i Safford 386 A		" 380 В	6.06		0.14	0.0196			
## Safford 490 A.		THE RES	5.80	200	0.12	0.0144		Library Co.	
## 402 A	i	Safford 386 A	3.87	3.92	0.05	0.0095	1 90	1 0901	0.000
2 Safford 490 B. 4.16 4.47 0.31 0.0961 0.84 0.7066 0.333 ., 439 A. 4.79 0.32 0.1024 4.45 0.02 0.0004 2 Safford 441 A. 5.77 4.62 1.15 1.3225 0.69 0.4761 0.333 ., 460 A. 4.34 0.28 0.0784 3.74 0.88 0.7744 3 Safford 490 A. 4.65 4.60 0.05 0.0025 0.71 0.5041 0.333 ., 495 A. 4.70 0.10 0.0100 4.44 0.06 0.036 2 Safford 501 B. 7.05 6.53 0.32 0.2704 1.22 1.4884 0.500 ., 513 A. 6.01 0.52 0.2704 3 Safford 525 A. 6.57 6.81 0.24 0.576 1.50 2.2500 0.333 ., 544 B. 6.57 0.24 0.0576 7.29 0.48 0.2304 4 Safford 556 B. 5.23 4.25 0.98 0.9604 1.06 1.1236 0.333 ., 562 A. 3.94 0.31 0.0961							1,00	1,3041	0.333
I Safford 430 B. 4.16 4.47 0.31 0.0961 0.84 0.7066 0.333 ,, 439 A. 4.79 0.32 0.1024 0.004 0.004 0.004 m Safford 441 A. 5.77 4.62 1.15 1.3225 0.69 0.4761 0.333 ., 460 A. 4.34 0.28 0.0784 0.744 0.88 0.7744 1' Safford 490 A. 4.65 4.60 0.05 0.0025 0.71 0.5041 0.333 ., 495 A. 4.70 0.10 0.0100 0.0036 <td></td> <td></td> <td>3.66</td> <td></td> <td>0.26</td> <td></td> <td></td> <td></td> <td></td>			3.66		0.26				
## Safford 441 A	,	Safford 490 D							
m Safford 441 A. 5.77 4.62 1.15 1.3225 0.69 0.4761 0.333 460 A. 4.34 0.28 0.0784 0.0784 1' Safford 490 A. 4.65 4.60 0.05 0.0025 0.71 0.5041 0.333 495 A. 4.70 0.10 0.0100 0.0100 0.0036 2' Safford 501 B. 7.05 6.53 0.52 0.2704 1.32 1.4884 0.500 3' Safford 525 A. 6.57 6.81 0.24 0.576 1.50 2.2500 0.333 ", 544 B. 6.57 0.48 0.2304 0.0576 1.22 1.4884 0.333 4' Safford 556 B. 5.23 4.25 0.98 0.9604 1.06 1.1236 0.333 ", 562 A. 3.94 0.31 0.0961 1.06 1.1236 0.333			100000	4.47		The state of the s	0.84	0.7056	0.333
m Safford 441 A		31 Day 21							
1' Safford 490 A					0.00	0.0004			
3.74 0.88 0.7744 1' Safford 490 A. 4.65 4.60 0.05 0.0025 0.71 0.5041 0.333 ", 495 A. 4.70 0.10 0.0100 4.44 0.06 0.0036 2' Safford 501 B. 7.05 6.53 0.52 0.2704 1.22 1.4884 0.500 ", 513 A. 6.01 0.52 0.2704 3' Safford 525 A. 6.57 6.81 0.24 0.576 1.50 2.2500 0.333 ", 544 B. 6.57 0.24 0.0576 7.29 0.48 0.2304 4' Safford 556 B. 5.23 4.25 0.98 0.9604 1.06 1.1236 0.333. ", 562 A. 3.94 0.31 0.0961	m		5.77	4.62	1.15	1.3225	0.69	0.4761	0.333
1' Safford 490 A		., 460 А				0.0784			
3' Safford 525 A. 6.57 6.81 0.24 0.576 1.50 2.2500 0.333 7.29 0.48 0.2304 4' Safford 556 B. 5.23 4.25 0.31 0.0961 0.005 0.71 0.3041 0.333 0.71 0.3041 0.333 0.71 0.3041 0.333 0.71 0.3041 0.333 0.71 0.3041 0.333 0.71 0.3041 0.333 0.71 0.3041 0.333 0.71 0.3041 0.333 0.71 0.3041 0.333 0.71 0.3041 0.333 0.304 0.304 0.304 0.304 0.304 0.333 0.31 0.3061			3.74		0.88	0.7744			
4.44 0.06 0.0036 2' Safford 501 B	1'	Safford 490 A	4.65	4.60	0.05	0.0025	0.71	0.5041	0.333
2' Safford 501 B		" 495 A	4.70		0.10	0.0100			
3' Safford 525 A 6.57 6.81 0.24 0.576 1.50 2.2500 0.833 , 544 B 6.57 0.24 0.0576 7.29 0.48 0.2304 4' Safford 556 B 5.23 4.25 0.98 0.9604 1.06 1.1236 0.833 , 562 A 3.94 0.31 0.0961			4.44		0.06	0.0036			
3' Safford 525 A 6.57 6.81 0.24 0.576 1.50 2.2500 0.333 , 544 B 6.57 0.48 0.24 0.0576 7.29 0.48 0.2304 4' Safford 556 B 5.23 4.25 0.98 0.9604 1.06 1.1236 0.333 , 562 A 3.94 0.31 0.0961	2'	Safford 501 B	7.05	6.58	0.52	0 9204	1 99	1 4884	0.500
3' Safford 525 A 6.57 6.81 0.24 0.576 1.50 2.2500 0.333 ,, 544 B 6.57 0.24 0.0576 7.29 0.48 0.2304 4' Safford 556 B 5.23 4.25 0.98 0.9604 1.06 1.1236 0.333 ,, 562 A 3.94 0.31 0.0961						2000	1	1.7001	0,000
4' Safford 556 B 5.23 4.25 0.31 0.0961 1.06 1.1236 0.333.	4								
7.29 0.48 0.2304 4' Safford 556 B 5.23 4.25 0.98 0.9604 1.06 1.1236 0.833. ,, 562 A 3.94 0.31 0.0961	9.			6.81			1.50	2.2500	0.333
4' Safford 556 B 5.23 4.25 0.98 0.9604 1.06 1.1236 0.833. ,, 562 A 3.94 0.31 0.0961		" 544 В							
" 562 A 3.94 0.31 0.0961			1.29		0.48	0,2301			
	4'	Safford 556 B	5.23	4.25	0.98	0.9604	1.06	1.1236	0.333.
3.59 0.66 0.4356		" 562 A	3.94		0.31	0.0961			
			3.59		0.66	0.4356	213		

Discusión—Continuación,

Pares.	Estrellas.	Latitud 31° 20′	Promedio.	Δ	Δ^2	Δφ	Δ φ 2	η
5'	Safford 571 A	6.66	7.13	0.47	0.2209	1.82	3.3124	0.333
	" 585 B	7.57		0.44	0.1936		lies in	
		7.17		0,04	0.0016			
6'	Safford 591 A	2.56	3.61	1.05	1.1025	1.70	2.8900	0.33
	., 604 A	4.28		0.67	0.4489			
		3.99		0.38	0.1444			
7' .	Safford 618 B	4.73	5.87	0.64	0.4096	0.06	0.0036	0.33
	" 626 A	5.53		0.16	0.0256		991	
		5.85		0.48	0.2304			
8'	Safford 637 A	7.13	6.15	0.98	0.9604	0.84	0.7056	0.33
	" 643 A	5.60		0.55	0.3025			
		5.71		0.44	0.1936			
9'	Safford 654 A	4.53	4.75	0.22	0.0484	0.56	0,3136	0.38
	" 658 C	4.99		0.24	0.0576			
		4.73		0.02	0.0004		-	
10'	Safford 670 B	4.33	4.53	0.20	0.0400	0.78	0.6084	0.88
	" 689 A	3.88		0.65	0.4225			
		5.38		0.85	0.7225			
11' -	Safford 721 A	5.14	5.84	0.34	0.1156	0.17	0.0289	0.50
	" 727 C	5.81		0.33	0.1089		Carrier Val	
12'	Safford 742 A	5.89	4.90	0.99	0.9801	0.41	0.1681	0.33
	" 755 A	4.72		0.18	0.0324			
		4.08		0.82	0.6724			
13'	Safford 764 B	6.55	6.93	0.38	0.1444	1.62	2.6244	0.50
	" 782 C	7.32		0.39	0.1521			
14'	Safford 784 A	6.16	5.77	0.39	0.1521	0.46	0.2116	0.8
	" 801 AA	5.50		0.27	0.0729			
		5.66	"	0.11	0.0121			
		Promedio.	5.31		28.7173		44.7961	13.99

El catálogo de los pares observados se encuentra en las páginas 215 y 216.

$$n=98$$
 $m=36$ $n-m=62$
 $e=0.6745$ $\sqrt{\frac{\Delta^2}{n-m}}=0.4593$ $e^2=0.2107$
 $E_{\varphi}^2=0.455$ $\frac{\Delta}{m}$ $e^2=0.5822$
 $e^2=\frac{e^2}{m-1}=0.0842$
 $e^2=\frac{e^2$



Pares.	Ecuaciones,	Pesos.	Pares.	Ecuaciones.	Pesos
1	φ - 7.10 d R - 6.19 = 0	0.80	h	φ - 8.97 d R - 5.92 = 0	
2	φ - 7.79 d R - 5.28 = 0	1.00	i	φ + 2.91 d R - 3.92 = 0	1.00
4	φ - 4.88 d R - 6.14 = 0	1.00	1	φ + 2.03 d R - 4.47 = 0	1.00
5	φ + 2.86 d R - 5.39 = 0	1.00	m	$\varphi - 1.85 \text{ d R} - 4.62 = 0$	1.00
6	φ - 9.74 d R - 6.96 = 0	1.00	1'	φ - 3.39 d R - 4.60 = 0	1.00
7	φ - 7.82 d R - 6.61 = 0	0.96	2'	$\varphi + 4.59 \text{ d R} - 6.53 = 0$	1.00
9	φ - 7.54 d R - 5.09 = 0	0.96	3'	$\varphi - 5.37 dR - 6.81 = 0$	0.96
10	φ - 1.06 d R - 5.06 = 0	1.00	4'	$\varphi + 9.29 \text{ d R} - 4.25 = 0$	1.00
11	φ + 0.93 d R - 4.09 = 0	1.00	5'	$\varphi - 14.59 \text{ d R} - 7.13 = 0$	1.00
12	φ + 8.12 d R - 5.70 = 0	1.00	6'	φ + 7.26 d R - 3.61 = 0	1.00
13	φ - 3.20 d R - 7.58 = 0	1.00	7'	$\varphi + 5.25 \text{ d R} - 5.37 = 0$	1.00
a	φ - 5.46 d R - 4.19 = 0	1.00	8'		1.00
b	φ - 5.39 d R - 5.29 = 0	0.96	9'	$\varphi - 8.13 dR - 6.15 = 0$	1.00
c	φ - 5.13 d R - 4.61 = 0	1.00	10'	$\varphi + 1.66 dR - 4.75 = 0$	1.00
d	φ + 4.91 d R - 3.41 = 0	1.00	11'	$\varphi - 4.73 dR - 4.53 = 0$	1.00
	φ - 4.16 d R - 6.43 = 0	0.96	12'	$\varphi - 5.26 dR - 5.48 = 0$	0.96
1	φ - 3.99 d R - 3.51 = 0	1.00	18'	$\varphi + 6.20 \text{ d R} - 4.90 = 0$	1.00
g	φ - 3.61 d R - 3.78 = 0	0.96	14'	φ - 7.20 d R - 6.93 = 0	0.96
		0.20	14	φ - 5.21 d R - 5.77 = 0	1.00

[a a. p] = + 35.52 [a b. p] = - 82.18 [a n. p] = - 188.23 [b b. p] = 950.36 [b b. p] = 1140.50 [b n. p] = 545.75 [b n. p] = 110.26 $\varphi = 5.03^{\circ}$ d R = - 0.116 $d R' = 9' \frac{1}{950.36}$ $\varphi' = \chi' = \frac{1}{29.60}$

Resultado final.

Pares.	Latitudes.	p	$p \varphi$	Δ	∇_3	p △2	Pares.	Latitudes.	P	Pq	Δ	∇_3	P
	"	0.00	4 400	0.40									
1	5.51	0.80	4.408	0.48	0.2304	0.1843	h	5.06	1.00	5.06	0.03	0.0009	0.00
2	4.53	1.00	4.530	0.50	0.2500	0.2500	i	4.20	1.00	4.90	0.83	0.6889	0.68
4	5.67	1.00	5.670	0.64	0.4096	0.4096	1	4.67	1.00	4.67	0.36	0,1296	0.12
5	5.66	1.00	5,660	0.63	0:3969	0.3969	m	4.49	1.00	4.49	0.54	0.2916	0.29
6	6.02	1.00	6.020	0.99	0.9801	0.9801	1'	4.28	1.00	4.28	0.75	0.5625	0.56
7	5.84	0.96	5.606	0.83	0.6889	0.6613	2'	6.97	0.96	6.091	1.94	3.7636	3.61
9	4.37	0.96	4.195	0.66	0.4856	0.4182	8'	6.29	1.00	6.29	1.26	1.5876	1.58
10	4.96	1.00	4.960	0.07	0.0049	0.0049	4'	5.14	1.00	5.14	0.11	0.0121	0.015
11	4.19	1.00	4.190	0.84	0.7056	0.7056	5'	5.73	1.00	5.78	0.70	0.4900	0.490
12	6.48	1.00	6.480	1.45	2.1025	2.1025	6'	4.31	1.00	4.81	0.72	0.5184	0.518
13	7.27	1.00	7.270	2.24	5.0176	5.0176	7'	5.87	1.00	5.87	0 84	0.7056	0.700
a ·	3.67	1.00	3.670	1.36	1.8496	1.8496	8'	5.87	1.00	5.87	0.34	0.1156	0.11
0	4.77	0.96	4.579	0.26	0.0676	0.0649	9'	4.91	1.00	4.91	0.12	0.0144	0.014
c	4.12	1.00	4.120	0.91	0.8281	0.8281	10'	4.08	1.00	4.08	0.95	0.9025	0.900
d	3.88	1.00	3.880	1.15	1.3225	1.3225	11'	4.97	0.96	4,771	0.06	0.0036	0.000
	6.03	0.96	5.789	1.00	1,0000	0.9600	12"	5.50	1.00	5.50	0.47	0.2209	0.220
f	3.13	1.00	3.130	1,90	3.6100	3.6100	13'	6.24	0.96	5.99	1.21	1.4641	1.400
g	3.43	0.96	3.293	1.60	2.5600	2,4576	14"	5.27	1.00	5.27	0.24	0.0576	0.057
	ALT SE							-	35.52			33,9894	33.544

 Latitud del punto de observación
 31° 20′ 5.03″ ± 0.11

 Reducción al Monumento 122
 = 4.06

 Latitud del Monumento 122
 31 20 0.97

Las latitudes puestas en la tabla de esta página, son las que resultan después de haber introducido en los cálculos la corrección encontrada arriba, para el valor angular de las revoluciones del tornillo micrométrico.

